Active Contours with Weighted External Forces for Medical Image Segmentation

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Abstract

Parametric active contours have been widely used for image segmentation. However, high noise levels and weak edges are the most acute issues that hinder their performance, particularly in medical images. In order to overcome these issues, we propose an external force that weights the gradient vector flow (GVF) field and balloon forces according to local image features. We also propose a mechanism to automatically terminate the contour’s deformation. Evaluation results on real MRI and CT slices show that the proposed approach attains higher segmentation accuracy than snakes using traditional external forces, while allowing initialization using a limited number of selected points.

1 Introduction

Parametric active contours, or snakes, model the movement of a dynamic curve towards an object’s boundary under the influence of internal and external forces [5, 8]. Parametric snakes produce closed and smooth object boundaries while allowing the separation of objects in contact by prohibiting contour fusions. The latter is an important advantage over non-parametric approaches, such as the level-set approach [15].

Despite the outstanding results of parametric snakes for image segmentation, their accuracy is relatively low when the amount of image clutter and noise is high [14]. In such cases, the use of various external forces that help the snake to conform to the desired boundary is an appropriate solution. For example, Cohen [2] propose balloon forces to guide the snake to the object’s boundary in a similar way a balloon inflates or deflates. Xu et al. [11] propose the gradient vector flow (GVF) field as an external force to help the snake to conform to concave boundaries. Other proposals include using vector field convolution (VFC) as an external force, which is calculated by convolving the image edge map with a user-defined vector field kernel [6]; integrating the GVF field with prior directional information manually provided [14]; convolving the image with a sigmoid function before computing the GVF field [12]; adaptively computing the GVF field according to the characteristics of an image region [10]; and computing a mean shift based GVF (MSGVF) to balance internal and external forces and drive the curve towards the desired boundary [13].

Although balloon forces may help guide the snake to the desired boundary over noise areas, the strength of the force must be appropriately set in order for the snake to detect weak edges and avoid snake leakages. GVF-based methods, and many of its variants, are proposed in order to address shortcomings of the balloon force; these external forces, however, may still require that the initial snake be initialized close to the desired boundary to obtain accurate segmentation results, particularly in noise images [1]. This inevitably involves manually...
selecting several initial points or snake elements. Moreover, regardless of the external force used, the appropriate number of iterations to accurately conform the desired boundary must be carefully selected in an empirical manner.

In this work, we propose an external force that combines the advantages of GVF and balloon forces, especially for cases when the snake is initialized far from the desired boundary in a noisy area and with a very limited number of snake elements. Specifically, balloon forces are used to guide the snake to the object’s boundary even in the presence of image clutter and noise; while GVF forces are used to improve segmentation accuracy even around weak edges. We control the effect of these two forces by a weighting function based on local image features. We also propose a mechanism to terminate the snake’s deformation process without having to manually indicate the number of iterations. The proposed approach minimizes snake leakages and considerably reduces the number of initial snake elements, making it suitable for medical image segmentation with little manual intervention.

2 Proposed External Force

A snake is a curve $C(s) = [x(s), y(s)]$, with $s \in [0, 1]$ at position $(x, y)$, that evolves to an object’s boundary by minimizing the energy functional $E_S = \int_0^1 [E_{int}(C(s)) + E_{ext}(C(s))] ds$, where $E_{int}(C(s)) = \frac{1}{2}(\alpha |C'(s)|^2 + \beta |C''(s)|^2)$ is the internal energy with $\alpha$ and $\beta$ controlling the smoothness of $C$, and $E_{ext}(C(s))$ is the external energy, which attracts $C$ towards the object’s boundary. $E_S$ can be minimized by evolving the snake dynamically as a function of parameter $s$ and artificial time $t$; namely, $C(s, t) = \left[ \alpha C'(s, t) - \beta C''(s, t) \right] - \nabla E_{ext}$. where the first term and the second term are called the internal force, $F_{internal}$, and the external force, $F_{external}$, respectively.

Our proposed external force is a weighted combination of balloon and GVF forces and aims at exploiting the advantages of each of these two forces. Balloon forces are represented as $F_{balloon} = n(s)$, where $n(s)$ is a unit vector normal to the snake at snake element $C_n$. GVF forces are derived from the diffusion of the gradient vectors of the image edge map $f(x, y)$, and are given as $F_{GVF} = v(x, y)$, where $v(x, y) = [u(x, y), v(x, y)]$ denotes the GVF field [11]. The proposed external force is then defined as $F_{external} = (F_{balloon} + (1 - \Omega)) + (F_{GVF} * \Omega)$, where $\Omega \in [0, 1]$ is a weighting factor given by:

$$\Omega = \bar{h}(1 - (AD - \varepsilon))$$

(1)

where $\bar{h} \in [0, 1]$ denotes the average intensity value of $f(x, y)$ over a semi-circular region $S$ of radius $r$ centered at each snake element, and $AD \in [0, 1]$ is the average angular difference between the direction of $F_{balloon}$ and the direction of the GVF field over a cone-shaped region $T$ centered at each snake element. $AD = 0$ represents 0 rad, while $AD = 1$ represents $\pi$ rad. Constant $\varepsilon = 0.001$ prevents power by zero when $AD = 1$. For each snake element at position $(x, y)$, $\bar{h}$ and $AD$ are calculated as follows:

$$\bar{h}(x, y) = \frac{1}{N} \sum_{(i, j) \in S} h(i, j); \quad AD(x, y) = \frac{1}{M * \pi} \sum_{(i, j) \in T} \theta(i, j)$$

(2)

where $N$ is the number of pixels located in region $S$, $h$ is the edge intensity at position $(i, j)$, $M$ is the number of GVF field vectors in region $T$, and $\theta$ is the minimum angle between the GVF field vector at position $(i, j)$ and $F_{balloon}$ for snake element $C_n$ at position $(x, y)$, as illustrated in Fig. 1. Note that $T(x, y, s, l, \varphi)$ is a cone-shaped region with its vertex in $(x, y)$, which allows analyzing the region located far from snake element $C_n$ and thus provides a better insight of the direction of the GVF field than the region close to $C_n$. 150
The weighting function in Eq. (1) assigns different priorities to $F_{balloon}$ and $F_{GVF}$ according to two local image features: the average edge intensity ($\bar{h}$) and the average GVF field direction ($\bar{AD}$). This weighting process helps to achieve the following:

1. Guide the snake to the boundary in smooth areas even if its normal direction of growth is opposite to $F_{GVF}$. This allows initialization far from the boundary with a limited number of snake elements. Fig. 2(a-b) illustrate this, where $\Omega$ approaches 0.
2. Minimize snake leakages around weak edges by averaging the edge intensity and the GVF field direction. Fig. 2(c) illustrates this, where $\Omega$ slowly approaches 1.
3. Conform to the desired boundary by assigning a higher weight to $F_{GVF}$ when edges are encountered. This is illustrated in Fig. 2(d), where $\Omega$ approaches 1.

In classical snakes, the deformation process is usually performed over a fixed number of iterations, over which it is expected to achieve convergence, i.e., external forces become zero. For images with strong edges, this number of iterations may be easily determined empirically. However, for images with weak edges, this number should be carefully selected to prevent leakages [7]. Here, we propose a mechanism to terminate the deformation process based on the percentage of snake elements labeled as off. A snake element is said to be off if no external force is acting on it. This usually occurs when the element encounters a strong edge, i.e., $F_{GVF}$ is the main acting external force ($\Omega > 0.5$) and the overall strength of the GVF field around the element is close to zero. To this end, if $\Omega > 0.5$, we compute $\Omega_b$ in the same manner as $\Omega$ in Eq. (1), but using regions $S_b$ and $T_b$, as illustrated in Fig. 3. We then label a snake element as off and set its forces to zero if $(\Omega_b)^2 > \Omega > 0.5$. This condition allows determining if the overall strength of the GVF field around the element is close to zero, i.e., the GVF field has opposite average directions in regions $T$ and $T_b$. We use the squared value of $\Omega_b$ to prevent the element from moving past the edge. If the percentage of off snake elements is equal to or greater than $Q$, the whole deformation process is terminated.

### 3 Experimental Results

The performance of the proposed approach over several regions of real MRI and CT slices is compared to that of snakes using three different external forces: a) $F_{GVF}$ exclusively [11], b) $F_{balloon}$ and image gradient (BGrad) forces [2], and c) $F_{GVF}$ or $F_{balloon}$ (BGVFT).
Figure 3: (a) Regions $T$ and $S$ (in red) used to compute $\Omega$, and regions $T_b$ and $S_b$ (in black) used to compute $\Omega_b$. (b) Dimension of regions $S$ and $S_b$ and of (c) regions $T$ and $T_b$.

Table 1: Detection accuracy of snakes using various external forces.

<table>
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<tr>
<th>Exp.</th>
<th>GVF</th>
<th>BGrad</th>
<th>BGVFT</th>
<th>Proposed</th>
<th>No. iterations</th>
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<tbody>
<tr>
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<td>DSC</td>
<td>JC</td>
<td>DSC</td>
<td>JC</td>
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<td>3</td>
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<td>0.9374</td>
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<tr>
<td>4</td>
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<td>0.8619</td>
<td>0.6844</td>
<td>0.5202</td>
<td>0.9231</td>
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</table>

according to a threshold i.e., if $\bar{h} > 0.05$ the acting external force is then set to $F_{\text{GVF}}$. All images are preprocessed using histogram equalization to enhance edges. The edge map $f(x, y)$ is computed using the wavelet coefficients obtained after applying the stationary wavelet transform (SWT) using the Haar filter with $L = 3$ levels of decomposition, as explained in [9]. We use all parameter values suggested in [11] to compute the GVF field and to control the snake’s smoothness. We use a radius $r = 1$ pixels for regions $S$ and $S_b$, an angle $\theta = 45^\circ$ and $sl = 5$ pixels for regions $T$ and $T_b$. These values provide the best trade-off between capturing enough local image features and computational complexity. All snakes are initialized inside the desired region by manually selecting a single position that is used as the center of an initial circular curve of $p$ pixels in radius. The whole deformation process is terminated if more than $Q = 90\%$ of the snake elements are labeled as off.

The detection accuracy of the evaluated methods is measured by the Dice similarity (DSC) [3] and Jaccard coefficients (JC) [4] using manually annotated ground truth. DSC and JC values are within the range $[0, 1]$, where 1 indicates identical overlap and 0 indicates no overlap between the regions inside the detected boundaries. Table 1 tabulates the DSC and JC values for different regions of MRI and CT slices. Experiments 1-3 represent three different regions of an MRI slice of a spinal cord, 4 and 5 represent two regions of an MRI slice of a pelvis, 6 and 7 represent two regions of an MRI slice of a knee, 8 represents one region of a CT slice of a skull, and 9 and 10 represent two regions of a CT slice of a spinal cord. In all experiments, the number of iterations is equal for all evaluated methods and is set to the number of iterations required by our termination mechanism. Results in Table 1 show that our approach achieves the highest accuracy for the majority of experiments. Note that for experiments 8-9, the BGVFT snake achieves higher DCS and JC values than our approach for the same number of iterations. In these cases, the BGVFT snake effectively switches between GVF and balloon forces based on the selected threshold. However, the
BGVFT snake, similarly to the GVF and BGrad snakes, requires manual selection of the number of iterations. More iterations may cause snake leakage, unlike our approach which terminates the deformation process when the majority of snake elements encounter strong edges. Visual results for experiment 2 are shown in Fig. 4. The BGrad snake conforms to the desired boundary with high accuracy (DSC=0.8969; JC=8130). However, for the same number of iterations required by our proposed approach, this snake does not reach the actual edge. More iterations may cause snake leakage around weak edges if the balloon force is greater than the gradient force. The GVF and BGVFT snakes result in leakages around weak edges. Our approach successfully conforms to the desired boundary with high accuracy.

Note that although the capture range of $F_{GVF}$ is in general large, methods using this external force exclusively may fail if the snake is initialized far from the desired boundary using a relatively small initial curve (see Fig. 5). The GVF field around such small initial snakes may not point towards the desired boundary due to the high levels of noise and clutter. An initial snake closer to the boundary may increase segmentation accuracy in this case.

### 4 Conclusion

This paper proposed an approach that combines balloon and GVF forces for parametric snakes, and a mechanism to automatically terminate the snake’s deformation process. The
approach uses a weighting factor to leverage the advantages of these two forces according to local image features. In smooth areas, balloon forces guide the snake to the object’s boundary, while in the presence of strong edge information GVF forces make the snake conform to the boundary. Experimental results on real medical images show that the proposed approach outperforms methods based on traditional external forces, while offering the advantage of initializing the snake with a single manually selected point inside the desired region and terminating the deformation process automatically.

References